

Quarterly Technical Report 77 - D

for

Hanford Seismic Network

October 1, 1977 through December 31, 1977

Geophysics Program

University of Washington

January 31, 1978

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PREPARED FOR THE U.S. DEPARTMENT OF ENERGY
UNDER CONTRACT NO. EY-76-S-06-2225
TASK AGREEMENT NO. 39

Operations

The eastern Washington seismic array has operated in the same configuration as at the end of last quarter. There have been few operational problems and only a few maintenance trips were required. The development and deployment of digital event recorders funded by WPPSS has proceeded with two stations currently operating in the Ellensburg area. Installation of these types of recorders in the more remote high mountain areas must be delayed until better weather.

Under development presently is a data base system on one of the University's general purpose computers to allow anyone in the state with a computer terminal to obtain any part of the latest catalog of located earthquakes. When this is operational all funding agencies will be notified of the procedures to obtain the data.

Data

The seismic activity in the Hanford region was below normal this quarter with only 15 events being located that are probably not blasts. The Entiat area was very active during this quarter with over twenty events in the immediate Entiat area. Several construction blasts in the area were recorded to help further define the velocity model. There were several earthquakes in the Ellensburg area though they did not occur when the digital event recorders were operating. The largest of these was a magnitude 2.9 on Oct. 9 and located about 5 km. NNE of Ellensburg.

Epicenter maps with this report show located earthquakes in figure 2 for this quarter, and probable and known explosions in figure 3.

Magnitude Calibration

We have relocated the Wood-Anderson instruments. On October 19th

and 20th, with the help of Mr. George Lest, a new location was found for the W-A instruments at the Battelle Northwest Office just outside Richland, Washington.

On November 30 the instruments were installed in the basement of the Battelle Northwest offices and are presently running at a magnification of 5600. The records are being changed by Mr. Harvey Hooker who is an electronic technician for Battelle. Mr. Tom Bishop has helped coordinate visits and necessary paper work.

We have recorded fifteen (15) local earthquakes at Entiat whose magnitudes can be computed. Several are very close to the Entiat station and the Richter magnitude could be questioned because of the short epicentral distance causing azimuthal dependency on ground motion amplitude.

To overcome this complexity we plan to inspect the Newport Observatory's Wood-Anderson records of selected earthquakes in northeastern Washington for comparison.

The seismicity in the Richland area is somewhat less than in the Entiat area and therefore it would seem that we may need to record longer at Richland to record a dozen or so magnitude determined earthquakes.

Tiltmeters

At the end of November, we thermally insulated the tiltmeter electronics and clamped the heavy cable between tiltmeters and their electronics packages. Clamping prevents any possible loading of the tiltmeters due to its cable. For the following month, all tiltmeters remained relatively quiet with maximum fluctuations of 0.8μ radians, which is a substantial improvement over the drift determined in the previous quarter.

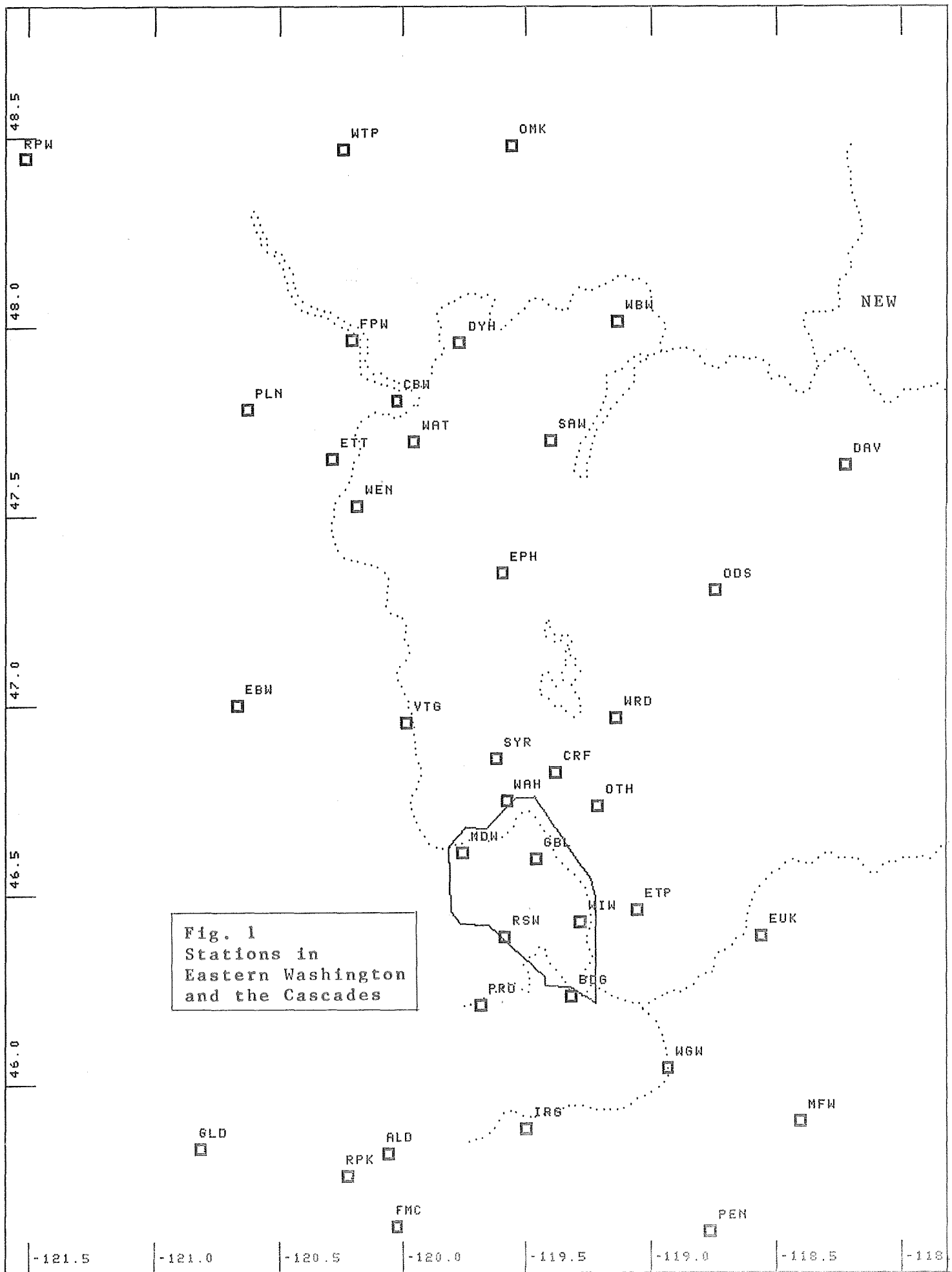
Using static loading near each tiltmeter, we determined the coordinate frame for each tiltmeter. However, the long term data is not in agreement

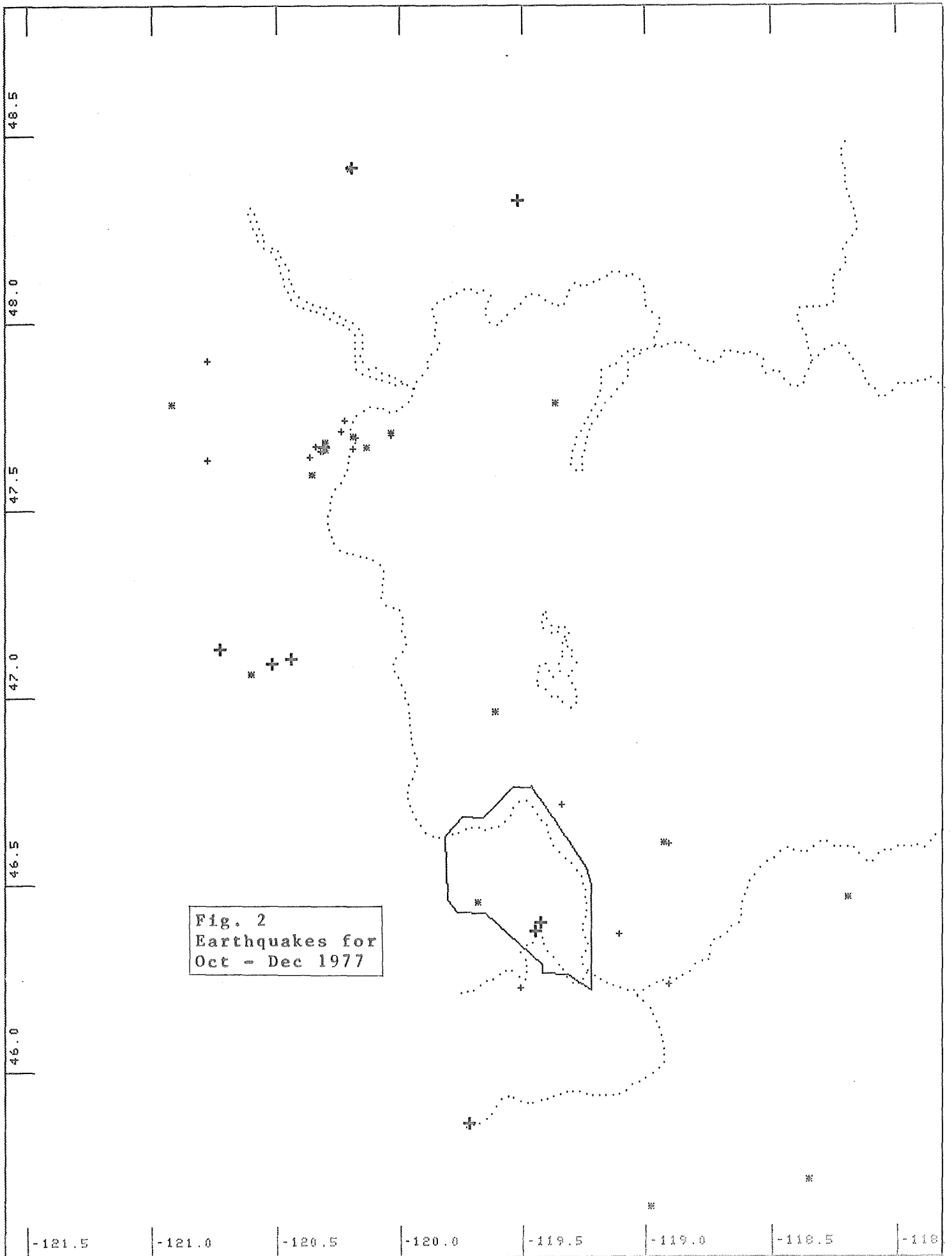
with the frame determined by the short term static loading. Using the frame determined by the short term loading, the long term easterly tilts and the long term northerly tilts track at a 180° phase difference between tiltmeters. We are currently trying to investigate the discrepancy between short term and long term data.

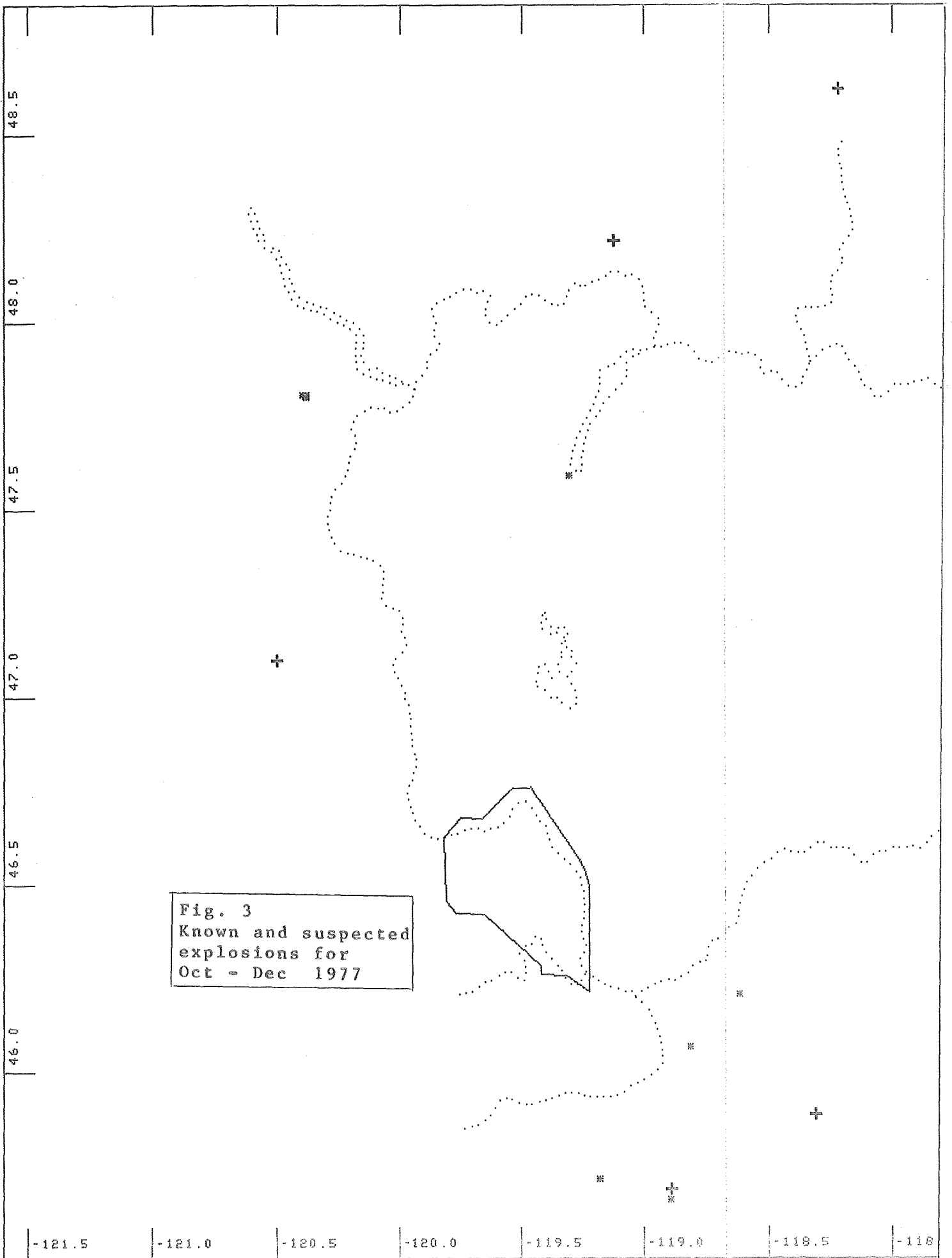
TABLE 1. Eastern Washington Velocity Models

North Model	<u>V_p</u> (km/sec)	<u>Depth</u>
	5.1	0.0
	6.05	0.5
	7.2	19.0
	8.0	24.5
South Model		
	3.7	0.0
	4.7	0.8
	5.15	1.2
	6.05	7.5
	7.2	19.0
	8.0	28.0

S - arrival times are computed by using the P - wave model and dividing the resulting travel time by 1.72.







Located with South Model

DATE	YRDAY	HRMN	SEC	N LAT	W LON	DEPTH	MAG	STA	GAP	ERR	ERZ	Q	TYPE
9/27/77	270	2043	4.0	45-53.20	118-18.64	1.0	2.4	7	271	4.0	2.8	D	P
9/30/77	273	2052	49.4	45-43.53	119- 9.90	3.0	1.7	5	224	10.7	13.3	D	P
10/ 6/77	279	2327	19.5	45-40.11	118-52.81	3.0	1.9	5	201	.2	.3	C	P
10/ 9/77	282	2320	8.6	45-43.05	118-20.17	1.7	2.0	6	265	2.8	.7	D	
10/20/77	293	1759	54.1	46-14.51	118-53.81	4.0	1.0	6	131	1.3	2.8	C	
10/20/77	293	2234	.9	45-38.83	118-57.95	1.8	1.7	6	240	8.7	10.0	D	
11/ 6/77	310	1720	1.8	46-27.52	119-40.01	20.9	1.4	12	195	1.3	1.3	C	
11/ 8/77	312	2223	32.1	45-51.65	119-43.25	.8	2.1	8	248	3.2	2.6	D	
11/10/77	314	16 7	40.3	46- 4.66	118-48.25	2.0	2.0	8	94	1.1	1.8	C	P
11/14/77	318	20 4	52.5	46-22.41	119-27.08	6.7	2.0	8	209	1.7	1.2	C	
11/18/77	322	9 8	37.8	46-22.59	119- 5.57	3.8	.6	9	147	.3	.4	E	
11/19/77	323	056	23.5	45-41.22	118-53.75	3.0	2.3	7	185	11.6	19.6	D	P
11/21/77	325	1952	55.3	46-23.43	118-10.72	4.9	1.9	6	298	4.1	1.5	D	
11/26/77	330	320	36.9	46-13.90	119-29.63	1.8	1.0	5	210	.7	13.5	D	
11/28/77	332	23 5	38.5	46-13.09	118-35.94	1.7	1.8	10	149	1.5	2.2	C	P
11/30/77	334	2330	1.8	46-47.93	119-45.05	3.0	2.0	8	233	37.1	21.8	D	
12/ 5/77	339	041	53.1	46-37.03	118-53.61	3.4	.9	8	192	1.2	1.9	C	
12/ 9/77	343	1627	17.3	46-37.14	118-54.79	.9	1.3	6	190	1.2	4.2	C	
12/13/77	346	932	14.2	46-58.22	119-35.79	3.0	2.0	17	80	.9	1.4	C	
12/21/77	355	218	19.1	46-23.94	119-26.08	1.5	2.3	11	88	.3	.6	C	
12/24/77	358	2 3	18.8	46-43.23	119-19.92	5.1	.3	7	227	1.1	2.2	C	

Located with North Model

DATE	YRDAY	HRMN	SEC	N LAT	W LON	DEPTH	MAG	STA	GAP	ERR	ERZ	Q	TYPE
7/ 7/77	188	2221	37.9	48-20.91	117-50.97	.3	1.8	6	183	1.5	3.7	C	P
7/10/77	191	719	31.3	48-30.41	122-31.66	4.0	3.9	10	329	17.6	25.4	D	W
7/13/77	194	715	6.2	47- 3.60	120-57.15	.1	3.8	28	67	1.1	2.7	D	F
7/13/77	194	720	1.5	47- 4.26	120-58.44	2.9	2.0	10	128	3.0	3.8	D	W
7/13/77	194	8 0	25.9	47-35.51	121-42.22	.1	2.4	9	82	2.2	11.2	C	W
7/13/77	194	1249	36.6	47- 4.19	120-59.20	.3	2.2	17	95	1.2	2.6	D	
7/13/77	194	1433	38.1	47- 3.85	120-59.11	1.0	2.4	17	96	1.2	1.9	D	
7/15/77	196	349	9.7	47-36.78	120-14.19	4.2	.5	9	142	.8	1.7	C	
7/15/77	196	630	.5	47-42.34	120- 7.43	4.3	.4	7	215	1.2	3.0	C	
7/15/77	196	1543	54.3	47-45.29	121-56.27	10.6	3.4	15	135	5.0	3.5	C	W
7/16/77	197	126	19.2	47-39.81	120-10.01	4.9	.5	6	156	1.6	6.6	C	
7/16/77	197	2 8	45.0	46-33.11	120-44.68	3.5	1.7	13	199	3.3	2.6	D	
7/17/77	198	1738	8.9	47- 6.33	120-59.06	5.5	1.5	6	277	14.6	3.4	D	
7/18/77	199	658	37.0	47-40.15	120-10.18	1.7	.9	7	153	.7	7.0	C	
7/22/77	203	622	42.9	47-42.25	120-15.60	6.8	.1	6	128	.3	.6	B	
7/23/77	204	1917	52.5	46-37.46	120-54.53	3.0	2.0	25	209	2.9	2.1	D	
7/25/77	206	522	19.5	47-40.61	120-18.88	1.6	-.3	7	150	.8	2.9	C	
7/27/77	208	1037	22.3	47-36.12	120-19.50	2.8	-.1	6	267	1.7	2.6	C	
7/29/77	210	5 0	27.1	47-37.79	120- 8.71	8.3	.5	9	136	.3	.6	B	
7/29/77	210	948	18.5	47-40.03	120-18.74	4.4	.1	8	149	.7	.9	B	
8/ 3/77	215	1437	9.4	47-11.89	119-52.30	3.0	1.0	5	130	1.6	48.7	D	
8/ 5/77	217	1447	55.1	48-20.44	120-49.87	3.0	1.3	7	265	3.9	90.3	D	
8/ 6/77	218	849	36.7	47-24.95	120-33.81	3.5	.5	7	287	5.3	41.7	D	
8/ 7/77	219	1532	11.2	47-37.20	120- 5.73	9.4	-.8	6	166	1.4	3.1	C	
8/ 9/77	221	124	15.2	47-39.37	120- 9.72	3.8	1.1	11	117	.3	1.4	B	
8/12/77	224	1731	46.6	47-36.72	120-22.56	6.0	-.4	6	191	.9	1.7	C	
8/14/77	226	0 0	56.9	47-44.26	120- 3.05	3.9	-.4	8	122	.9	2.0	B	
8/18/77	230	3 3	14.4	47-39.91	120-18.93	1.7	-.6	5	175	1.5	4.7	C	
8/20/77	232	1110	43.1	47-41.21	120- 4.10	8.8	1.3	14	120	.4	.8	B	
8/23/77	235	452	16.5	47- 3.64	120-58.70	.6	1.7	12	156	.8	15.5	D	
8/28/77	240	737	17.6	48-44.31	119-51.33	5.4	1.6	11	279	2.5	2.0	C	
8/29/77	241	1240	38.8	47-43.11	120-17.10	8.1	2.8	18	101	1.0	.9	B	
8/30/77	242	2116	54.7	47-39.36	120-11.06	7.1	.3	7	108	.2	.6	B	
9/ 1/77	244	2 1	3.0	47-17.12	119-50.59	9.1	1.3	11	247	.8	.7	C	
9/ 1/77	244	2311	7.7	48-40.38	120-16.18	2.1	1.4	10	277	3.3	30.5	D	
9/ 2/77	245	043	46.0	48-40.65	120-16.07	3.2	1.1	10	278	2.6	1.9	D	
9/ 4/77	247	1810	30.4	47-43.35	120- 2.48	7.2	-.0	7	136	.5	1.1	B	
9/ 5/77	248	043	22.8	47- 5.91	121- 1.65	3.0	1.6	18	154	2.2	1.7	D	
9/ 5/77	248	524	46.6	47- 6.01	121- .73	2.0	1.6	15	154	2.2	2.0	D	
9/11/77	254	1244	8.9	48- 8.12	119-10.32	.9	1.7	8	206	1.8	3.7	C	
9/14/77	257	854	45.0	47-41.80	120-22.63	3.0	-.4	8	171	1.0	4.7	C	
9/16/77	259	622	17.0	47-37.21	120-17.29	2.9	.2	6	160	1.7	5.5	C	
9/17/77	260	125	5.4	47-37.86	120-14.73	4.6	.8	11	139	1.0	3.0	C	
9/17/77	260	945	32.7	48-53.71	119-17.12	.1	2.1	11	297	2.2	2.2	D	
9/20/77	263	527	11.4	47-39.73	120-16.19	.1	.8	8	87	.9	1.5	B	
9/22/77	265	1459	11.9	47-38.23	120-19.12	.0	1.2	13	162	.5	.9	C	
9/23/77	266	2110	51.3	47-42.96	120-47.98	6.2	.7	5	318	5.3	5.5	D	
9/27/77	270	124	17.1	47-40.40	120- 8.92	6.1	-.9	7	131	.2	.9	B	
9/28/77	271	240	41.3	47-40.09	120- 4.30	7.7	-.5	6	196	.7	1.5	C	
9/28/77	271	20 3	47.9	47-48.91	120-21.38	3.0	-.1	6	132	1.1	15.4	C	

Located with North Model

DATE	YRDAY	HRMN	SEC	N LAT	W LON	DEPTH	MAG	STA	GAP	ERR	ERZ	Q	TYPE
10/ 6/77	279	951	6.2	47-43.18	120-13.54	3.0	.6	9	119	.5	2.7	B	
10/ 9/77	282	116	47.0	47-40.15	120-17.32	1.8	1.6	13	104	.4	1.5	B	
10/ 9/77	282	255	16.0	47- 5.51	120-31.18	.3	2.9	20	216	1.5	2.1	D	
10/10/77	283	1155	13.8	47-47.72	119-21.25	.1	1.5	6	165	1.0	3.6	C	
10/10/77	283	1528	17.5	47-40.78	120-19.39	7.9	.6	10	147	.4	.5	B	
10/12/77	285	0 3	16.9	47-48.84	120-22.36	9.8	1.4	14	135	.4	.7	B	X
10/16/77	289	2359	26.8	47-41.37	120-17.34	2.3	1.8	12	107	.4	1.8	B	
10/18/77	291	1938	3.2	47-47.48	120-54.63	.5	1.2	7	313	1.8	77.7	D	
10/19/77	292	116	38.9	47-45.09	120- .94	3.9	-1.1	9	153	.5	1.0	B	
10/19/77	292	23 6	34.8	47-49.12	120-22.60	.5	1.7	14	138	.8	28.0	C	X
10/21/77	294	2331	8.3	47-36.07	119-17.71	4.7	1.6	7	156	.6	2.9	C	P
10/22/77	295	831	57.2	47-39.11	120-21.12	5.9	.1	8	166	.3	.3	B	
10/22/77	295	1418	42.9	47-42.32	120-10.64	6.7	1.7	12	70	.6	2.1	B	
10/23/77	296	8 0	15.0	48-25.38	120-10.93	3.0	1.3	11	124	1.0	4.5	B	
10/23/77	296	922	18.3	48-25.04	120-11.64	.1	2.1	12	121	.2	2.6	B	
10/23/77	296	1518	53.5	47- 6.08	120-30.00	1.8	2.2	13	214	1.6	2.9	C	P
10/26/77	299	034	33.6	47-48.74	120-21.99	.5	1.7	10	133	.7	54.8	C	X
10/26/77	299	122	22.3	47-40.03	120-17.88	1.5	.0	6	132	1.8	4.9	B	
10/26/77	299	1334	2.9	47-42.59	120- 1.43	7.2	.6	9	150	.2	.6	B	
10/26/77	299	15 8	37.4	47-40.03	120-18.19	.8	.1	6	147	1.7	9.9	C	
10/28/77	301	425	40.2	47-41.76	121-39.91	1.0	2.0	6	331	6.8	3.8	D	W
10/28/77	301	1016	4.1	47-42.87	120- 1.44	7.6	1.3	15	71	.3	.4	A	
11/ 1/77	305	537	12.3	47-45.42	120- 6.78	8.2	-1.4	8	111	.4	.8	B	
11/ 1/77	305	1210	45.1	47-36.32	120-20.10	4.8	1.1	9	183	.5	1.7	C	
11/ 2/77	306	1958	31.4	47-48.97	120-22.07	.5	1.4	9	135	.7	66.4	C	X
11/ 3/77	307	424	22.8	47-40.42	120-10.54	6.9	.3	9	104	.3	.7	B	
11/ 3/77	307	17 8	44.5	47- 4.40	120-35.33	5.8	2.0	8	273	2.4	2.8	C	
11/ 4/77	308	441	57.7	47-43.52	120-18.61	1.8	-1.4	5	114	.4	4.1	C	
11/ 4/77	308	2344	58.0	47-41.15	120-15.61	7.3	-1.4	7	150	.5	.7	B	
11/ 5/77	309	2150	54.9	47-48.78	120-21.90	3.0	1.1	7	133	.6	9.2	C	X
11/ 8/77	312	1211	10.5	47- 7.75	120-43.96	8.6	2.2	13	233	1.7	1.4	C	
11/13/77	317	1926	17.9	47-38.64	120-46.02	16.3	.6	7	305	1.4	1.4	C	
11/15/77	319	051	15.4	47-48.83	120-21.94	.5	1.4	7	133	.8	58.0	C	X
11/17/77	321	2314	56.7	47-48.78	120-21.83	.5	1.1	7	132	.5	2.3	C	X
11/18/77	322	1231	23.8	48-19.57	119-31.12	6.5	2.7	11	151	.5	1.1	B	
11/23/77	327	555	3.1	47-42.24	120- 7.34	7.9	-1.1	8	103	.5	1.4	B	
11/23/77	327	21 7	56.0	47-48.96	120-22.04	.5	1.5	8	134	.4	81.5	C	X
11/24/77	328	1136	34.8	47-54.47	120-46.00	3.0	.8	7	297	2.5	20.0	D	
12/ 7/77	341	045	45.2	47-48.86	120-22.29	.5	1.6	8	135	.6	19.9	C	X
12/ 7/77	341	2018	34.6	47-44.85	120-12.58	3.0	0.0	7	148	.4	3.1	C	
12/ 9/77	343	858	16.1	47-40.65	120- 7.08	5.5	1.1	11	120	.5	1.7	B	
12/ 9/77	343	1946	22.6	48-13.28	119- 7.43	.2	2.5	10	243	1.1	3.4	C	P
12/10/77	344	1326	16.5	47-42.27	120- 9.63	8.2	.1	8	149	.7	1.7	B	
12/21/77	355	027	11.9	48-37.60	118-13.28	1.5	2.0	8	297	3.6	2.1	D	P
12/22/77	356	647	57.5	47-40.22	120-18.61	6.6	2.3	13	147	.6	1.2	B	
12/27/77	361	1850	36.0	47-42.42	121-46.37	6.1	1.9	8	337	12.0	3.0	D	W
12/28/77	362	1340	50.1	47- 6.18	120-26.47	3.0	2.1	12	209	1.9	29.9	D	
12/30/77	364	149	46.6	47-44.45	120- 4.74	7.3	-1.5	8	123	.3	.6	B	

Located with South Model

DATE	YRDAY	HRMN	SEC	N LAT	W LON	DEPTH	MAG	STA	GAP	ERR	ERZ	Q	TYPE
7/ 3/77	184	11 4	51.7	46-42.71	119-31.53	.0	.7	7	113	.3	.6	B	
7/ 4/77	185	056	39.7	46-50.69	119-28.21	6.9	-.1	5	250	.2	.1	C	
7/ 5/77	186	1128	49.0	46-48.21	119-32.27	3.0	1.6	9	137	1.1	1.8	C	
7/ 5/77	186	14 7	35.2	46-48.87	119-33.27	1.5	1.2	11	142	1.0	2.7	C	
7/ 5/77	186	15 6	15.5	46-48.59	119-32.56	4.5	.4	6	225	1.0	.7	C	
7/ 6/77	187	2137	46.0	46-12.28	119-16.50	1.5	1.4	7	313	1.0	1.1	C	P
7/ 7/77	188	1432	21.3	46-27.43	119-33.67	18.4	.4	5	122	2.7	2.1	D	
7/13/77	194	1429	22.1	46-29.75	120- 2.81	14.2	.6	6	311	.8	1.8	C	
7/14/77	195	516	56.7	46-42.46	119-31.09	7.1	.3	6	122	.8	.8	B	
7/15/77	196	1554	9.2	46-53.88	119-38.62	7.6	1.7	17	89	1.2	2.6	C	P
7/17/77	198	2356	6.3	46- 7.80	119-27.65	1.5	2.2	10	129	.6	.9	C	P
7/19/77	200	2110	40.9	46-43.93	119-15.36	.6	.8	11	77	.6	1.3	B	
7/19/77	200	2252	55.3	45-25.83	118-38.25	3.0	2.1	7	306	8.2	2.7	D	P
7/20/77	201	1651	59.3	46- 8.06	119-27.81	.3	1.9	10	160	.5	1.1	B	P
7/20/77	201	2113	59.5	46-38.98	119-37.74	7.9	1.0	7	131	1.5	7.3	C	P
7/21/77	202	1518	23.3	46- 7.63	119-27.49	.8	2.2	8	196	.7	3.6	C	P
7/21/77	202	1929	52.9	46- 4.98	119-26.59	3.4	1.6	7	278	4.0	2.8	D	P
7/24/77	205	1520	46.5	46-38.88	119-18.55	11.9	-.1	6	182	.8	2.1	C	
7/29/77	210	18 5	59.9	46-52.94	119-22.10	.8	.5	7	276	7.0	5.1	D	
8/ 1/77	213	2030	8.6	46- 8.24	119-27.08	15.9	.9	5	292	1.3	.7	D	
8/ 3/77	215	1716	7.1	45-44.29	118- 5.70	5.5	2.1	7	298	2.5	4.3	C	P
8/ 6/77	218	2018	6.5	46-50.99	119-23.48	1.3	.5	4	260	0.0	0.0	C	
8/ 7/77	219	857	42.9	46-42.64	119-31.41	3.9	.4	6	119	.2	.8	B	
8/10/77	222	3 4	59.3	45-12.73	118-13.72	1.5	2.0	6	327	6.7	7.1	D	R
8/12/77	224	1816	54.6	46-50.89	119-10.68	3.5	1.3	11	157	.7	.8	B	P
8/16/77	228	1652	38.7	46-22.44	119-33.36	18.7	.6	7	232	2.0	1.2	C	
8/18/77	230	443	52.2	46-39.06	119-37.60	.8	1.2	11	74	1.0	2.0	C	
8/19/77	231	2017	31.9	46-42.41	119-30.89	3.0	.9	7	124	.3	2.6	B	
8/23/77	235	133	25.5	46-42.33	119-31.50	4.8	.2	7	119	.2	.7	B	
8/23/77	235	2347	55.1	45-54.11	119-19.15	.3	1.9	11	124	.5	1.0	B	
8/24/77	236	1220	38.5	46-42.18	119-31.28	.2	1.0	8	121	.3	.7	B	
8/25/77	237	1740	43.1	46-50.98	119-10.58	3.0	1.8	12	161	1.1	1.4	C	P
9/ 2/77	245	425	20.7	46-38.31	119-21.28	16.6	.4	8	89	.7	1.3	A	
9/ 9/77	252	1440	15.4	46-42.15	119-32.27	3.0	0.0	5	112	.9	6.3	D	
9/11/77	254	413	15.9	46-38.48	119-37.73	1.5	2.7	15	69	1.0	2.0	C	
9/11/77	254	450	26.2	46-38.85	119-37.78	3.0	-.1	7	130	.5	4.6	C	
9/11/77	254	511	6.2	46-38.95	119-38.08	.8	-.3	8	133	.5	1.0	B	
9/14/77	257	1345	9.5	46-49.04	119-32.90	4.0	.6	7	132	.5	1.7	B	
9/14/77	257	14 5	56.9	46-51.61	119-33.64	10.2	.5	8	192	1.7	1.7	C	
9/14/77	257	1925	52.4	46-49.09	119-33.10	3.0	.9	9	132	.7	2.8	B	
9/16/77	259	019	31.7	46-42.54	119-31.82	6.9	.3	7	116	.7	.7	B	